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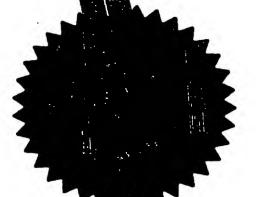
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Description

Claim(s) Abstract

Drawing(s)

10. If you are also filing any of the following, state how many against each Item.

Priority documents

Translations of priority documents

Statement of inventorship and right to grant of a patent (Patents Form 7/77)

Request for preliminary examination and search (Patents Form 9/77)

Request for substantive examination (Patents Form 10/77)

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11.

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PCT / GB 02 / 02633 describes a jet injector in which there is a rigid tube terminating at one end in a nozzle and at the other in a constriction which leads to the main drug supply. A portion of the rigid tube is formed as a flexible window. There is an over centre spring which may deliver a hammer blow to the window to cause a high speed flow through the nozzle and a more gradual acceleration of drug through the constriction. The jet pierces the skin of the patient to cut a track and the main dose may be delivered manually down this track. The present specification details a number of improvements in the design of this device

According to the present invention, there are a number of improvements to the jet injector specified in PCT / GB 02 / 02633 which are as follows. Rather than energising the spring by pressing against the skin of the patient, the profile of load with displacement may be made asymmetric so that the spring is energised manually and triggered by pressure on the skin of the patient. The spring may be in the form of one of more C springs deforming by bending in the plane of the axis of the injector. The C profile may be modified toward an L or J shape if required. The C spring may be retained by a cross member that seats in a transverse channel at the base of a retaining wall. The cross member may engage with the flexible portion of the rigid tube via a small cross section piston. The flexible portion of the rigid wall may be formed as a rubber liner within the rigid tube that is accessed via an open window within the rigid tube wall. The rubber liner may incorporate a non-return valve that is normally closed or is biassed in the closed position. The rubber liner may be free or bonded to the constriction for ease of assembly. The outer surface of the nozzle may be such that it induces a saddle shape in the skin it impresses in order to maintain the entrance to the track through the skin in the open position.

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In the original specification, it was stipulated that the device was energised by pressure against the skin of the patient. The spring reached the unstable maximum strain configuration then spontaneously accelerated to impact. There was facility within the design to constrain the load-displacement profile of the spring between the limits of travel. If these limits are set extremely asymmetrically, the spring is effectively energised by manually cocking the device and then triggered by pressure against the skin of the patient. As human fingers have evolved to comfortably exert much larger forces that most of the skin, this arrangement permits a much larger spring energy and reduced loading on the skin of the patient. This arrangement also provides greater design flexibility within the limited space available.

The spring outlined in PCT / GB 02 / 02633 deformed by shear and stretching. Such an arrangement on a small scale leads to a rigid spring design of limited deflection and limited energy. The limited deflection leads to difficult fabrication tolerances. Bending strain offers greater deflection and the potential for greater energy storage. In the cited priority documents, circular springs are described which bend about two axes simultaneously. White such devices provide greater flexibility, the biaxial bend constraint substantially reduces the energy that may be stored within the material strain limits. A C spring provides bending strain but in one plane only. Figure 1a shows such a spring, 106, in side view and in end elevation in figure 1b. There are two C shaped elements, which are disposed symmetrically about the injector body, and are bonded rigidly by cross beams, 104 and 110, at their ends. One cross beam, 110, pivots freely while the other is attached rigidly a triangular cross member, 105, which may pivot in a transverse channel, 107, to extend the spring. Figure 1c shows



the C spring in the extended mode. The restraining wall, 108, prevents further rotation and the rear wall of the pivot channel, 107, provides a reaction, so that the spring assembly is securely retained.

The configuration of figure 1c is clearly at maximum spring strain. By placing the 5 lower pivot point, 121, slightly forward of the pivot channel, 107, a forward rotation moment is generated which latches the spring against the restraining wall, 108. It is important there is no bending moment between the spring, 106, and the cross member, 105, that upsets this latching. During the stretching of the C spring, there is rotation 10 of the cross member, bodily rotation of the spring and splaying of the spring. In figures 1d and 1e, the initial and final spring curvatures are shown schematically as curves 102 and 103 respectively. Figure 1d shows the bodily rotation angle, 101. Figure 1e shows the splay angle, 100, on extension of the spring. It may be shown that the angle between the cross member and spring first decreases then increases with 15 extension of the spring. There is always a configuration at full extension where there is no change in this angle and therefore no additional bending moment due a distortion of the angle between cross member and spring.

While C springs have been considered so far, the profile of the spring may be redesigned as closer to an L or J configuration, without changing the essential mechanics. This may permit a larger spring in a confined design space.

In PCT/GB02/02633 a double sided system is presented. A single sided system offers more design flexibility and eliminates timing problems on impact.

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The end thrust member, 105, may have a peg, 109, of small smaller cross section that may act as a piston driving the flexible window, 111, in a hole of similar size. In this fashion a given impact force may produce a much higher impact pressure within the rigid tube.

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To form a flexible window, 111, within the wall of a rigid tube, 120, requires a delicate priming and moulding operation with the risk of flash, 130, within the channel. The flash may break away to block the nozzle, 131. A simpler arrangement is shown in section in figure 2. There is an open window, 20, in the rigid wall, 9, and a rubber liner, 21, within the rigid tube. When the piston impacts on the liner, the pressure within the tube increases, reinforcing the seal of the liner against the innex surface of the rigid tube wall. The forces on the liner are essentially isotropic, so despite the extremely high hydraulic pressure transient, there will be no damage to the rubber. The liner may also incorporate a slit non-return valve, 22. This may be closed in the quiescent state or even biassed in the closed position by the seating pressure of the rubber liner. With such a valve, there can be no reverse flow down the constriction, 23, so the transient pressure will be higher and the volume pumped through the nozzle will be greater. Further, thermal contraction of fluid in the attached drug ampoule cannot withdraw fluid from the pump chamber so ambient thermal cycling will not interfere with priming of the pump. The liner cum non-return valve may be free standing but is preferably bonded to the inner face of the constriction, 23. The constriction is still required to given support to the non return valve and ensure a small dead volume on the pump stroke. However, the length may be attenuated as there is no longer the need to have a large column of fluid to impede acceleration of the reverse flow. The rubber is preferably silicone and a 20%

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addition of silicone oil prior to cure to ensure that the valve does not re-seal during storage. The non-return valve may be opened by the syringe piston pressure to deliver the main dose in the normal fashion.

The outer surface of the nozzle may induce a saddle shape in the skin under pressure. 5 Skin is remarkably resistant to biaxial stretching so to ensure that the slit like orifice to the track through the skin is held open, the stress must be anisotropic. Figure 3 shows a nozzle surface, 30, that is essentially conical, 31, with a cylindrical relief, 32, perpendicular to the injector axis. The skin, 33, is extended under pressure by forming around the cylindrical surface. This tension keeps the track entrance, 34, 10 open.

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Abstract

PCT / GB 02 / 02633 describes a low cost jet injector. The present specification describes a number of improvements in the device. The spring may be manually cocked and pressure on the skin of the patient may trigger the energy release. The spring may be in the form of one or more C springs deforming by bending solely in the plane of the injector axis. The end thrust beams may comprise a discrete piston that engages with a small cross section cylinder. A small channel provides a simple detent mechanism to retain the spring. The flexible portion of the rigid tube may be formed by having an open window in the rigid tube with a cylindrical shell rubber moulding within the tube. This moulding may be free or bonded onto the end of the constriction. The moulding may also incorporate a non return valve that is normally closed or even biassed closed in the quiescent state. The outer surface of the nozzle may be saddle shaped to keep the track entry open.

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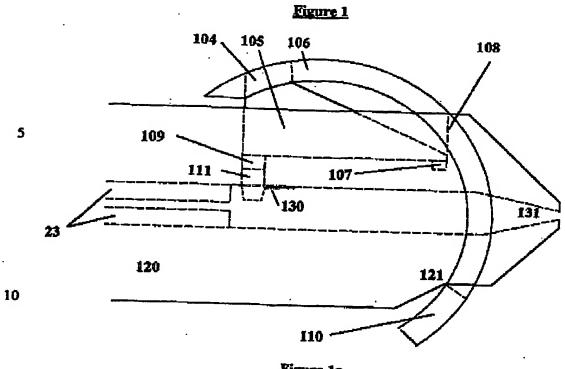
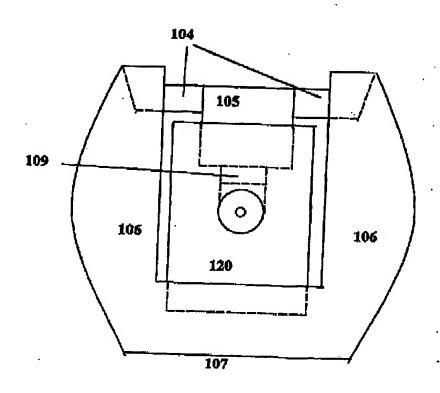


Figure 1a

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Figure 1b

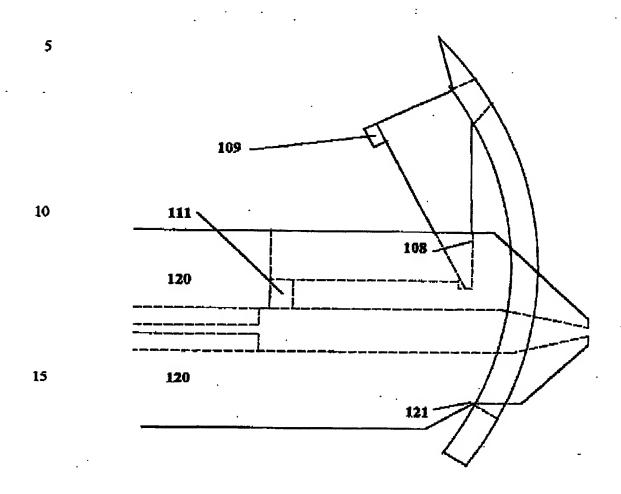


Figure 1c

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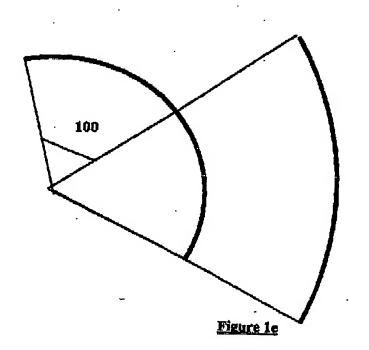
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Figure 1d

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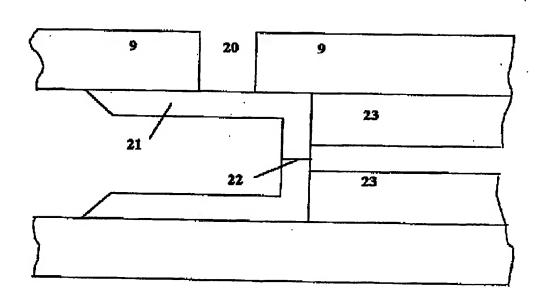
Figure 2

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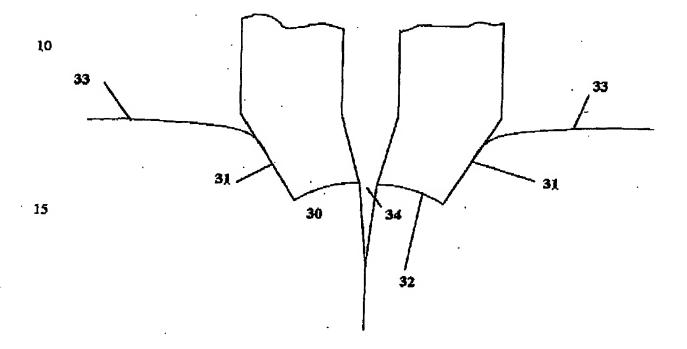




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Figure 3

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